

COMPARISON OF PHYSICAL-CHEMICAL PROPERTIES AND DEGRADATION RATES OF PCB-28 AND PCB-180 BETWEEN INDIVIDUAL MODELS

Table B.1. “Reference data sets” of physical-chemical properties and degradation rates of PCB-28 and PCB-180*

Description		Numerical values		Comments	Reference
		PCB-28	PCB-180		
Air/water Henry's law constant, K_H (Pa·m ³ /mol)					
Temperature dependent: $H = H_0 \exp (-a_H (1/T - 1/T_0))$ where T - temperature (K), H_0 is the value at the reference temperature T_0 , and a_H is a parameter of temperature dependence.	H_0 (T_0), Pa·m ³ /mol	9.46E+00	1.98E+00	Coefficients are recalculated from the following temperature dependence: $\log H = \log H(25^\circ\text{C}) - (\Delta U_{aw} + R \cdot 298.15)/(\ln(10) \cdot R) \cdot (1/T - 1/298.15)$ where: T - temperature; R - Universal Gas Constant; ΔU_{aw} - internal energy of phase transfer, kJ/mol (PCB-28: 52.3; PCB-180: 63.6). $H(25^\circ\text{C})$ - Henry 's law constant at 25°C, Pa·m ³ /mol (PCB-28: 30.5; PCB-180: 8.13).	Li et al., 2003
	a_H	6588.7	7947.9		
Air/water partition coefficient, K_{aw} (dimensionless)					
Temperature dependent: $K_{aw} = K_{aw}^0 \exp (-a_{Kaw}(1/T - 1/T_0))$ where T - temperature (K), K_{aw}^0 is the value at the reference temperature T_0 , and a_{Kaw} is a parameter of temperature dependence.	K_{aw}^0 (T_0), dimensionless	4.02E-03	8.42E-04	Coefficients are recalculated from the following temperature dependence: $\log K_{aw} = \log K_{aw}(25^\circ\text{C}) - \Delta U_{aw}/(\ln(10) \cdot R) \cdot (1/T - 1/298.15)$ where: T - temperature; R - Universal Gas Constant; ΔU_{aw} - internal energy of phase transfer, kJ/mol (PCB-28: 52.3; PCB-180: 63.6). $K_{aw}(25^\circ\text{C})$ - dimensionless air/water partition coefficient at 25°C, estimated from: $K_{aw}(25^\circ\text{C}) = H(25^\circ\text{C})/(R \cdot 298.15)$	Li et al., 2003
	a_{Kaw}	6290.6	7649.7		
Subcooled liquid vapour pressure, p_{ol} (Pa)					
Temperature dependent: $p_{ol} = p_{ol}^0 \exp (-a_p(1/T - 1/T_0))$ where T - temperature (K), p_{ol}^0 is the value at the reference temperature T_0 , and a_p is a parameter of temperature dependence.	p_{ol}^0 (T_0),	5.24E-03	1.51E-05	Coefficients are recalculated from the following temperature dependence: $\log p_{ol} = \log p_{ol}(25^\circ\text{C}) - (\Delta U_a + R \cdot 298.15)/(\ln(10) \cdot R) \cdot (1/T - 1/298.15)$ where: T - temperature; R - Universal Gas Constant; ΔU_a - internal energy of phase transfer, kJ/mol (PCB-28: 74.2; PCB-180: 89.6). $p_{ol}(25^\circ\text{C})$ - vapour pressure at 25°C, Pa (PCB-28: 2.70E-2; PCB-180: 1.08E-4).	Li et al., 2003
	a_p	9222.9	11075.2		
Octanol/water partition coefficient, K_{ow} (dimensionless)					
Temperature dependent: $K_{ow} = K_{ow}^0 \exp (a_{Kow}(1/T - 1/T_0))$ where T - temperature (K), K_{ow}^0 is the value at the reference temperature T_0 , and a_{Kow} is a parameter of temperature dependence.	K_{ow}^0 (T_0), dimensionless	8.09E+05	2.70E+07	Coefficients are recalculated from the following temperature dependence: $\log K_{ow} = \log K_{ow}(25^\circ\text{C}) - \Delta U_{ow}/(\ln(10) \cdot R) \cdot (1/T - 1/298.15)$ where: T - temperature; R - Universal Gas Constant; ΔU_{ow} - internal energy of phase transfer, kJ/mol (PCB-28: -26.3 ; PCB-180: -29.1). $K_{ow}(25^\circ\text{C})$ - octanol/water partition coefficient at 25 °C, dimensionless (PCB-28: 4.61E+5; PCB-180: 1.45E+7)	Li et al., 2003
	a_{Kow}	3163.3	3500.1		

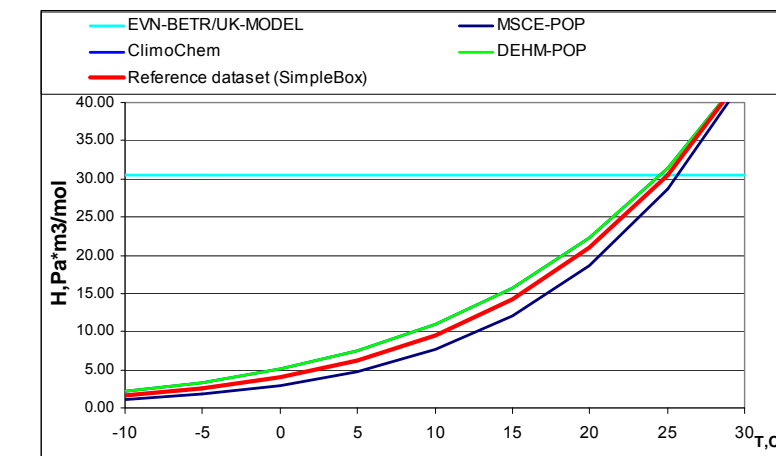
Description		Numerical values		Comments	Reference
		PCB-28	PCB-180		
Octanol/air partition coefficient, K_{oa} (dimensionless)					
Temperature dependent: $K_{oa} = K_{oa}^0 \exp (a_{Koa}(1/T - 1/T_0))$ where T - temperature (K), K_{oa}^0 is the value at the reference temperature T_0 , and a_{Koa} is a parameter of temperature dependence.	$K_{oa}^0 (T_0)$, dimensionless	3.77E+08	1.06E+11	Coefficients are recalculated from the following temperature dependence: $\log K_{oa} = \log K_{oa}(25^{\circ}\text{C}) - \Delta U_{oa}/(\ln(10) \cdot R) \cdot (1/T - 1/298.15)$ where: T - temperature; R - Universal Gas Constant; ΔU_{oa} - internal energy of phase transfer, kJ/mol (PCB-28: -78.5; PCB-180: -92.8). $K_{oa}(25^{\circ}\text{C})$ - octanol/air partition coefficient at 25°C, dimensionless (PCB-28: 7.05E+7; PCB-180:1.46E+10);	Li et al., 2003
	a_{Koa}	9441.9	11161.9		
Organic carbon/water partition coefficient, K_{oc} (dimensionless)					
Regression relation: $K_{oc} = \text{regc } K_{ow}^b$ where regc and b are regression coefficients	regc	0.41	0.41	K_{oc} is calculated from K_{ow} , where K_{ow} is the temperature dependent octanol-water partition coefficient	Karickhoff, 1981
	b	1	1		
Water solubility, S_{WL} (mol/m ³)					
Temperature independent	$S_{WL} (T)$, mol/m ³	5.53E-04	7.57E-06	Values are calculated for $T = 283.15$ with the help of the following temperature dependence: $\log S_{WL} = \log S_{WL}(25^{\circ}\text{C}) - \Delta U_W/(\ln(10) \cdot R) \cdot (1/T - 1/298.15)$ where: R - Universal Gas Constant; ΔU_W - internal energy of phase transfer, kJ/mol (PCB-28: 22.0; PCB-180: 26.0). $S_{WL}(25^{\circ}\text{C})$ - water solubility, mol/m ³ at 25°C (PCB-28: 8.85E-4; PCB-180:1.32E-5).	Li et al., 2003
Degradation rate constants, k_d (1/s)					
Degradation in atmosphere: Temperature independent	$k_{air} (T)$, 1/s	3.50E-07	3.50E-08	Degradation rate constant in the air is conversed from half-life values, h (PCB-28: 550; PCB-180: 5500): $k_d = 0.693/ t_{1/2}$ where k_d is the first-order rate constant (s ⁻¹) and $t_{1/2}$ is the half-life (s).	Mackay et al, 1992
Degradation in soil: Temperature independent	$k_{soil} (T)$, 1/s	3.50E-09	3.50E-09	Degradation rate constant in soil is conversed from half-life values (PCB-28:55000; PCB-180: 55000): $k_d = 0.693/ t_{1/2}$ where k_d is the first-order rate constant (s ⁻¹) and $t_{1/2}$ is the half-life (s).	Mackay et al, 1992
Degradation in water: Temperature independent	$k_{water} (T)$, 1/s	1.13E-08	3.50E-09	Degradation rate constant in water is conversed from half-life values (PCB-28: 17000; PCB-180: 55000): $k_d = 0.693/ t_{1/2}$ where k_d is the first-order rate constant (s ⁻¹) and $t_{1/2}$ is the half-life (s).	Mackay et al, 1992
Degradation in sediment: Temperature independent	$k_{sed} (T)$, 1/s	3.50E-09	3.50E-09	Degradation rate constant in sediment is conversed from half-life values (PCB-28: 55000; PCB-180: 55000): $k_d = 0.693/ t_{1/2}$ where k_d is the first-order rate constant (s ⁻¹) and $t_{1/2}$ is the half-life (s).	Mackay et al, 1992

* - for the sake of comparability, the base values and coefficients of temperature dependences of the considered parameters are given here for the temperature 283.15 K (T_0) and the way they were recalculated from original dependencies is specified in the field "Comments".

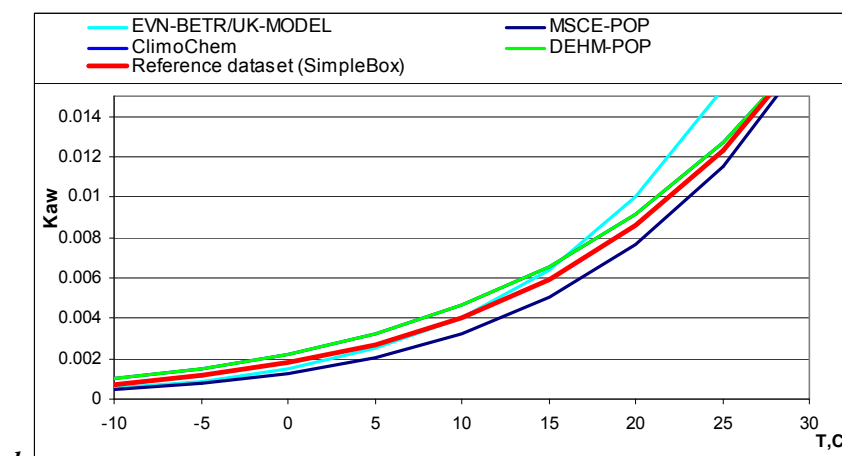
Table B.2. The Henry's law constant and the air/water partition coefficient of PCBs (data sets of the participating POP models)*

Model	Description	Numerical values			Comments	Reference
			PCB-28	PCB-180		
CAM/POPs	Temperature dependent: $H = H_0 \exp (- a_H (1/T - 1/T_0))$ where T - temperature (K), H_0 is the value at the reference temperature T_0 , and a is a parameter of temperature dependence. Temperature dependent: $K_{aw} = H / (R \cdot T)$	H_0 , Pa·m ³ /mol	-	2.53E-01	Coefficient a_H of the exponential equation are recalculated from the coefficient of the following temperature dependence: $H = H_0 \cdot 10^{(- 3416 (1/T - 1/T_0))}$ with the help of the following formula: $a_H = \ln(10) \cdot 3416$, It was obtained from the following temperature dependence: $\log(H/H(25^{\circ}\text{C})) = \text{slop} (1/T - 1/ 298)$ $H(25^{\circ}\text{C})$ - Henry 's law constant at 25 ⁰ C, Pa·m ³ /mol (PCB-180: 1.01)	Achman, Hornbuckle, Eisenreich [1993]
		a_H	-	7865.6		
		T_0 , K	-	283.15		
SimpleBox	Temperature dependent: $H = H_0 \exp (- a_H (1/T - 1/T_0))$ where T - temperature (K), H_0 is the value at the reference temperature T_0 , and a_H is a parameter of temperature dependence.	H_0 , Pa·m ³ / mol	9.46E+00	1.98E+00	Same to the “reference data set”	Li et al., 2003
		a_H	6588.7	7947.9		
		T_0 , K	283.15	283.15		
EVN-BETR and UK-MODEL	H is temperature independent.	H , Pa·m ³ /mol	30.5	8.18	Calculated as $H = \text{Vapour Pressure (Pa)} / \text{Water Solubility (mol/m}^3\text{)}$ at 25 ⁰ C	Li et al., 2003
	Temperature dependent: $K_{aw} = K_{aw}^0 \exp (- a_{Kaw}(1/T - 1/T_0))$ where T - temperature (K), K_{aw}^0 is the value at the reference temperature T_0 , and a_{Kaw} is a parameter of temperature dependence.	K_{aw} , dimensionless	4.02E-03	8.48E-04	At 10 ⁰ C, calculated as: $K_{aw}(T_0) = 10^{\log K_{aw}} \cdot a$, $a = \exp[(\Delta H_{vap} / R) \cdot (1 / T_0 - 1 / T)]$. $\Delta H_{vap} = 62.8$ kJ/mol: Enthalpy of vaporisation (from water to air) Here $a_{Kaw} = \Delta H_{vap} / R$	
		a_{Kaw}	7553.5	7553.5		
		T_0 , ⁰ K	283.15			
CliMoChem	Temperature dependent: $K_{aw} = K_{aw}^0 \exp (- a_{Kaw}(1/T - 1/T_0))$ where T - temperature (K), K_{aw}^0 is the value at the reference temperature T_0 , and a_{Kaw} is a parameter of temperature dependence.	K_{aw} , dimensionless	4.63E-03	1.83E-03	$K_{aw}(T) = K_{aw}(T_{ref}) \exp(dH_{Kaw}/R(1/T_{ref} - 1/T))$ (dimensionless) T = temperature (283.15 K); T_{ref} = reference temperature (298.15 K) $K_{aw}(T_{ref})$ = Henry 's law constant at T_{ref} (dimensionless): PCB 28: 1.27E -2 ; PCB 180: 8.92E-3 dH_{kaw} = phase transfer enthalpy (J/mol): PCB 28: 47200; PCB 180:74100 R = universal gas constant (8.3145 J/mol·K)	Beyer et al., 2002
		a_{Kaw}	5680	8910		
		T_0 , K	283.15			
DEHM-POP	Temperature dependent: $K_{aw} = K_{aw}^0 \exp (- a_{Kaw}(1/T - 1/T_0))$ where T - temperature (K), K_{aw}^0 is the value at the reference temperature T_0 , and a_{Kaw} is a parameter of temperature dependence.	K_{aw} , dimensionless	4.63E-03	1.83E-03	$K_{aw}(283.15) = K_{aw}^0(298.15) \exp (-a_{Kaw}(1/T - 1/T_0))$, where $K_{AW}^0(298.15) = 1.27\text{E-}2, 8.92\text{E-}3$ for PCB 28 and 180 respectively	Beyer at al., 2002
		a_{Kaw}	5680	8917		
		T_0 , K	283.15			
MSCE-POP	Temperature dependent: $H = H_0 \exp (- a_H (1/T - 1/T_0))$ where T - temperature (K), H_0 is the value at the reference temperature T_0 , and a_H is a parameter of temperature dependence. Temperature dependent: $K_{aw} = H / (R \cdot T)$	H_0 , Pa·m ³ /mol	7.642	2.388	Coefficients of the exponential equation are recalculated from the standard form of temperature dependence: $\log H = -A/T(K) + B$ with the help of the following formulas: $a_H = \ln(10) \cdot A$; $H_0 = 10^{(-A/T_0 + B)}$, where $A = \Delta H_W / 2.303R$; $B = \log H_{298} + \Delta H_W / 2.303R(298)$. where H_{298} is Henry's law constant (Pa·m ³ /mol) at 25 ⁰ C (PCB-28: 28.58; PCB-180: 10.74); ΔH_W is the enthalpy of volatilization from water, kJ/mol (PCB-28: 61.8; PCB-180: 71.3)	Burkhard et al., 1985 Dunnivant et al., 1992
		a_H	7430	8575		
		T_0 , K	283.15	283.15		

* - for the sake of comparability, the base values and coefficients of temperature dependences of the considered parameters are given here at the temperature 283.15 K (T_0) and the way they were recalculated from original dependencies is specified in the field "Comments".

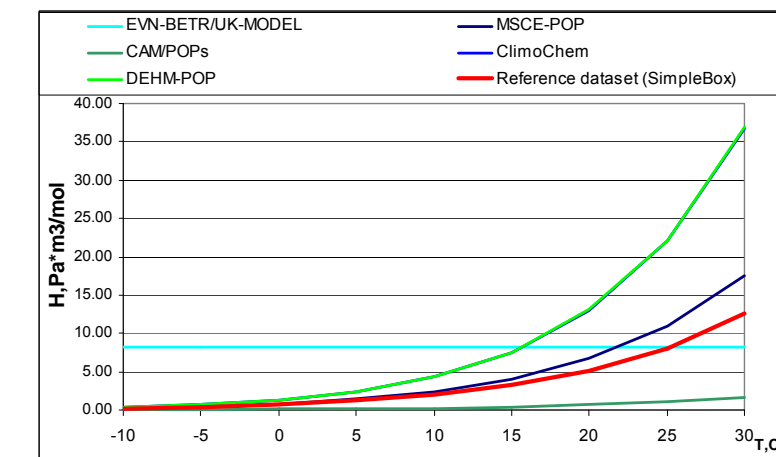


a

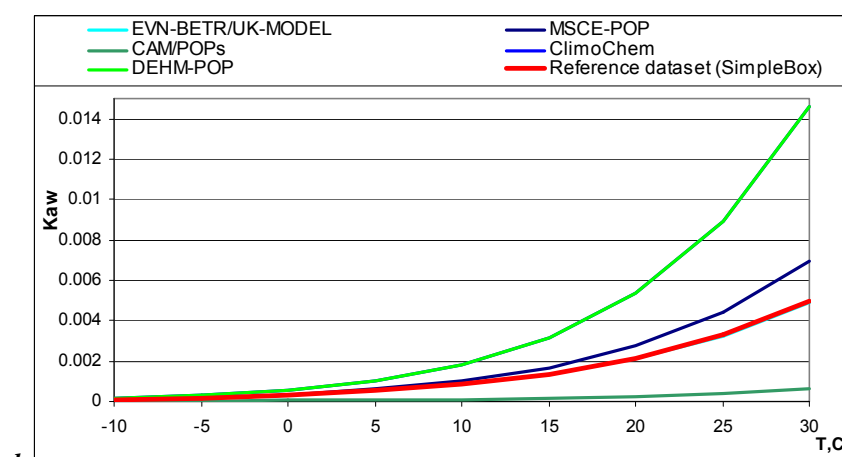


b

Fig. B.1. Comparison of temperature dependencies of Henry's law constant (H , $\text{Pa}\cdot\text{m}^3/\text{mol}$) and air/water partition coefficient (K_{aw} , dimensionless) of PCB-28.



a



b

Fig. B. 2. Comparison of temperature dependencies of Henry's law constant (H , $\text{Pa}\cdot\text{m}^3/\text{mol}$) and air/water partition coefficient (K_{aw} , dimensionless) of PCB-180.

Table B.3. Absolute values and statistical parameters of Henry's law constant (H , Pa·m³/mol) and air/water partition coefficient (K_{aw} , dimensionless) of PCB-28 for three arbitrary temperatures (-10°C, 10°C and 25°C) and coefficients of temperature dependencies

	H , Pa·m ³ /mol				K_{aw} , dimensionless			
	-10°C	10°C	25°C	a_H	-10°C	10°C	25°C	a_{Kaw}
SimpleBox	1.61E+00	9.46E+00	3.05E+01	6588.7	7.43E-04	4.02E-03	1.23E-02	6290.6
EVN-BETR and UK-MODEL	3.05E+01	3.05E+01	3.05E+01	-	5.29E-04	4.02E-03	1.54E-02	7553.5
CliMoChem	2.21E+00	1.09E+01	3.15E+01	-	1.01E-03	4.63E-03	1.27E-02	5680
DEHM-POP	2.21E+00	1.09E+01	3.15E+01	-	1.01E-03	4.63E-03	1.27E-02	5680
MSCE-POP	1.04E+00	7.64E+00	2.86E+01	7430	4.75E-04	3.25E-03	1.15E-02	-
"Reference data set"	1.61E+00	9.46E+00	3.05E+01	6588.7	7.43E-04	4.02E-03	1.23E-02	6290.6
min	1.04E+00	7.64E+00	2.86E+01	6588.7	4.75E-04	3.25E-03	1.15E-02	5680.0
max	3.05E+01	3.05E+01	3.15E+01	7430.0	1.01E-03	4.63E-03	1.54E-02	7553.5
arith. mean	6.53E+00	1.31E+01	3.05E+01	6869.1	7.51E-04	4.09E-03	1.28E-02	6298.9
median	1.91E+00	1.02E+01	3.05E+01	6588.7	7.43E-04	4.02E-03	1.25E-02	6290.6
geom. mean	2.72E+00	1.16E+01	3.05E+01	6858.0	7.22E-04	4.07E-03	1.28E-02	6263.9
max/min	2/29*	1/4*	1	1.1	2	1	1	1.3

* - the first value is calculated without the temperature independent value of H (EVN-BETR and UK-MODEL), the second value is calculated taking it into account.

Table B.4. Absolute values and statistical parameters of Henry's law constant (H , Pa·m³/mol) and air/water partition coefficient (K_{aw} , dimensionless) of PCB-180 for three arbitrary temperatures (-10°C, 10°C and 25°C) and coefficients of temperature dependencies

	H , Pa·m ³ /mol				K_{aw} , dimensionless			
	-10°C	10°C	25°C	a_H	-10°C	10°C	25°C	a_{Kaw}
CAM/POPs	3.06E-02	2.53E-01	1.02E+00	7865.6	1.40E-05	1.07E-04	4.13E-04	-
SimpleBox	2.35E-01	1.98E+00	8.13E+00	7947.9	1.08E-04	8.42E-04	3.28E-03	7649.7
EVN-BETR and UK-MODEL	8.18E+00	8.18E+00	8.18E+00	-	1.12E-04	8.48E-04	3.25E-03	7553.5
CliMoChem	3.66E-01	4.31E+00	2.21E+01	-	1.67E-04	1.83E-03	8.91E-03*	8910*
DEHM-POP	3.66E-01	4.31E+00	2.21E+01	-	1.67E-04	1.83E-03	8.92E-03*	8917*
MSCE-POP	2.39E-01	2.39E+00	1.10E+01	8575	1.09E-04	1.01E-03	4.42E-03	-
"Reference data set"	2.35E-01	1.98E+00	8.13E+00	7947.9	1.08E-04	8.42E-04	3.28E-03	7649.7
min	3.06E-02	2.53E-01	1.02E+00	7865.6	1.40E-05	1.07E-04	4.13E-04	7553.5
max	8.18E+00	8.18E+00	2.21E+01	8575.0	1.67E-04	1.83E-03	8.92E-03	8917.0
arith. mean	1.38E+00	3.34E+00	1.15E+01	8084.1	1.12E-04	1.04E-03	4.64E-03	8136.0
median	2.39E-01	2.39E+00	8.18E+00	7947.9	1.09E-04	8.48E-04	3.28E-03	7649.7
geom. mean	3.32E-01	2.32E+00	8.40E+00	8079.2	9.20E-05	8.05E-04	3.38E-03	8111.6
max/min	12/267***	17/32***	22/22***	1.1	12	17	22	1.2

*- difference in absolute values obtained from identical temperature dependencies can be explained by accuracy of coefficient recalculation.

*** - the first value is calculated without the temperature independent value of H (EVN-BETR and UK-MODEL), the second value is calculated taking it into account.

Table B.5. The subcooled liquid vapour pressure of PCBs (data sets of the participating POP models)*

Model	Description	Numerical values			Comments	Reference
			PCB-28	PCB-180		
CAM/POPs	Temperature dependent: $p_{ol} = p_{ol}^0 \exp(-a_p(1/T - 1/T_0))$ where T - temperature (K), p_{ol}^0 is the value at the reference temperature T_0 , and a_p is a parameter of temperature dependence.	p_{ol}^0 , Pa	-	1.67E-05	Coefficients of the exponential equation are recalculated from the standard form of temperature dependence: $p_{ol} = 10^{(m/T + b)}$ where T - temperature ($^{\circ}$ K); $m = -5042$ - parameter of temperature dependence, and $b = 13.03$ - parameter depended on molecular weight. It was obtained from the following original equation: $\log(p_{ol}) = -Q / (2.303 RT) + b$ where: T - temperature; R - Universal Gas Constant; Q - the heat of vaporisation (kJ/mol)	Harner et al., 1996; Falconer et al., 1995
		a_p	-	11610		
		T_0 , K	-	283.15		
SimpleBox	Temperature dependent: $p_{OL} = p_{OL}^0 \exp(-a_p(1/T - 1/T_0))$ where T - temperature (K), p_{OL}^0 is the value at the reference temperature T_0 , and a_p is a parameter of temperature dependence.	p_{OL}^0 , Pa	5.24E-03	1.51E-05	Same to the "reference data set"	Li et al., 2003
		a_p	9222.9	11075.2		
		T_0 , K	283.15	283.15		
EVN-BETR and UK-MODEL	Temperature independent:	p_{OL} , Pa	2.70E-02	1.08E-04	T = 25°C	Li et al., 2003
MSCE-POP	Temperature dependent: $p_{ol} = p_{ol}^0 \exp(-a_p(1/T - 1/T_0))$ where T - temperature (K), p_{ol}^0 is the value at the reference temperature T_0 , and a_p is a parameter of temperature dependence.	p_{OL}^0 , Pa	6.43E-03	1.67E-05	Coefficients of the exponential equation are recalculated from the standard form of temperature dependence: $\log p_{ol}(\text{Pa}) = -A/T(K) + B$ with the help of the following formulas: $a_p = \ln(10) \cdot A$ $p_{ol}^0 = 10^{(-A/T_0 + B)}$ where; $A = 4075$ and 5072 for PCB-28 and PCB-180 respectively; $B = 12.20$ and 13.03 for PCB-28 and PCB-180 respectively	Falconer and Bidleman, 1994
		a_p	9383	11610		
		T_0 , K	283.15	283.15		

* - for the sake of comparability, the base values and coefficients of temperature dependences of the considered parameters are given here at the temperature 283.15 K (T_0) and the way they were recalculated from original dependencies is specified in the field "Comments".

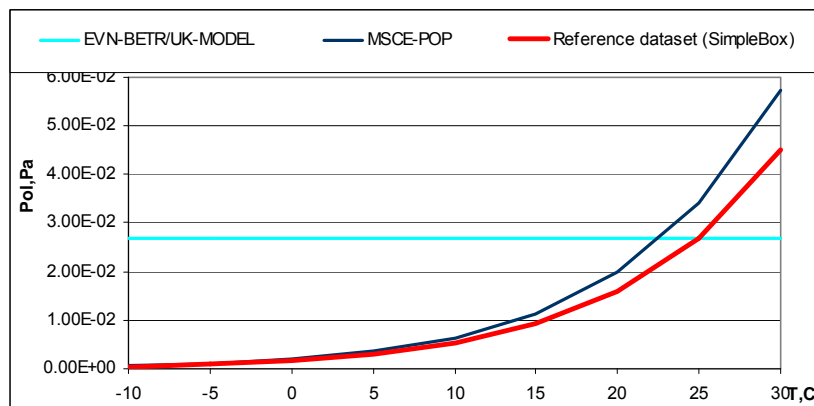


Fig. B.3. Comparison of temperature dependencies of subcooled liquid vapour pressure of PCB-28 used in data sets of the participating POP models and in “reference data set”

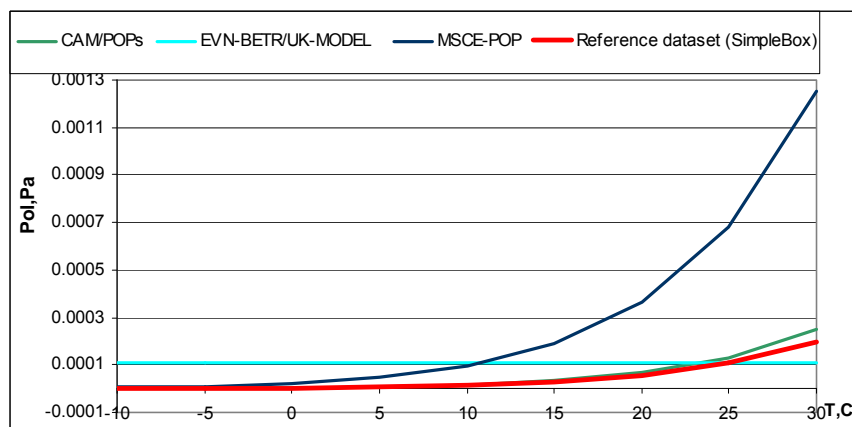


Fig. B.4. Comparison of temperature dependencies of subcooled liquid vapour pressure of PCB-180 used in data sets of the participating POP models and in “reference data set”

Table B.6. Absolute values, coefficients of temperature dependence and statistical parameters of subcooled liquid vapour pressure of PCB-28 for three arbitrary temperatures (-10 °C, 10 °C and 25 °C)

	p_{0L} , Pa			a_p
	-10°C	10°C	25°C	
SimpleBox	4.41E-04	5.24E-03	2.70E-02	9222.9
EVN-BETR/UK-MODEL	2.70E-02	2.70E-02	2.70E-02	-
MSCE-POP	5.18E-04	6.43E-03	3.41E-02	9383
Reference data set	4.41E-04	5.24E-03	2.70E-02	9222.9
<i>min</i>	4.41E-04	5.24E-03	2.70E-02	9222.9
<i>max</i>	2.70E-02	2.70E-02	3.41E-02	9383.0
<i>arith. mean</i>	7.10E-03	1.10E-02	2.88E-02	9276.3
<i>median</i>	4.79E-04	5.84E-03	2.70E-02	9222.9
<i>geom. mean</i>	1.28E-03	8.31E-03	2.86E-02	9276.0
<i>max/min</i>	1.2/61.3*	1.2/5.2*	1.3	1.02

* - the first value is calculated without the temperature independent value of p_{0L} (EVN-BETR and UK-MODEL), the second value is calculated taking it into account

Table B.7. Absolute values, coefficients of temperature dependence and statistical parameters of subcooled liquid vapour pressure of PCB-180 for three arbitrary temperatures (-10 °C, 10 °C and 25 °C)

	p_{0L} , Pa			a_p
	-10°C	10°C	25°C	
CAM/POPs	7.40E-07	1.67E-05	1.31E-04	11610
SimpleBox	7.73E-07	1.51E-05	1.08E-04	11075.2
EVN-BETR/UK-MODEL	1.08E-04	1.08E-04	1.08E-04	-
MSCE-POP	5.07E-06	9.69E-05	6.84E-04	11610
Reference data set	7.73E-07	1.51E-05	1.08E-04	11075.2
<i>min</i>	7.40E-07	1.51E-05	1.08E-04	11075.2
<i>max</i>	1.08E-04	1.08E-04	6.84E-04	11610.0
<i>arith. mean</i>	2.31E-05	5.04E-05	2.28E-04	11342.6
<i>median</i>	7.73E-07	1.67E-05	1.08E-04	11342.6
<i>geom. mean</i>	3.00E-06	3.31E-05	1.62E-04	11339.4
<i>max/min</i>	6.8/145.9*	6.4/7.2*	6.3	1.05

* - the first value is calculated without the temperature independent value of p_{0L} (EVN-BETR and UK-MODEL), the second value is calculated taking it into account

Table B.8. The octanol/water partition coefficient of PCBs (data sets of the participating POP models)*

Model	Description	Numerical values			Comments	Reference
			PCB-28	PCB-180		
CAM/POPs	Temperature dependent: $K_{ow} = K_{oa} \cdot H/RT$ where T - temperature (K); R - Universal Gas Constant; H - Henry's law constant; K_{oa} - Octanol/air partition coefficient (dimensionless)		-	-	These values are calculated with the help of temperature dependencies of H and K_{oa} .	This study
SimpleBox	Temperature dependent: $K_{ow} = K_{ow}^0 \exp(a_{Kow}(1/T - 1/T_0))$ where T - temperature (K), K_{ow}^0 is the value at the reference temperature T_0 , and a_{Kow} is a parameter of temperature dependence.	$K_{ow}^0(T_0)$, dimensionless	8.09E+05	2.70E+07	Same to the "reference data set"	Li et al., 2003
		a_{Kow}	3163.3	3500.1		
		T_0, K	283.15	283.15		
EVN-BETR and UK-MODEL	Temperature dependent: $K_{ow} = K_{ow}^0 \exp(a_{Kow}(1/T - 1/T_0))$ where T - temperature (K), K_{ow}^0 is the value at the reference temperature T_0 , and a_{Kow} is a parameter of temperature dependence.	K_{ow}^0 , dimensionless	8.02E+05	2.69E+07	For 10°C, calculated as $K_{ow}(T_0) = 10^{\log K_{ow}} \cdot a$, $a = \exp[(\Delta H_{sol}/R) \cdot (1/T_0 - 1/T)]$. $\Delta H_{sol} = -31.1$ KJ/mol: Enthalpy of solution (from octanol to water) Here: $a_{Kow} = \Delta H_{sol}/R$	Li et al., 2003
		a_{Kow}	3740.5	3740.5		
		T_0, K	283.15	283.15		
CliMoChem	Temperature dependent: $K_{ow} = K_{ow}^0 \exp(a_{Kow}(1/T - 1/T_0))$ where T - temperature (K), K_{ow}^0 is the value at the reference temperature T_0 , and a_{Kow} is a parameter of temperature dependence ($-dH/R$)	K_{ow}^0 , dimensionless	9.41E+05	1.84E+07	$K_{ow}(T) = K_{ow}(T_{ref}) \exp((dHK_{ow}/R)(1/T_{ref} - 1/T))$ dimensionless T = temperature (283.15 K); T_{ref} = reference temperature (298.15 K) $K_{ow}(T_{ref})$ = Octanol/water partition coefficient at T_{ref} PCB 28: 5.13E+5; PCB 180: 1.54E+7 dHK_{ow} = phase transfer enthalpy (J/mol) PCB 28: -28400; PCB 180: -8270 R = universal gas constant (8.3145 J/mol·K)	Beyer et al., 2002
		a_{Kow}	3415.7	994.6		
		T_0, K	283.15	283.15		
DEHM-POP	Temperature dependent: $K_{ow} = K_{ow}^0 \exp(a_{Kow}(1/T - 1/T_0))$ where T - temperature (K), K_{ow}^0 is the value at the reference temperature T_0 , and a_{Kow} is a parameter of temperature dependence ($-dH/R$)	K_{ow}^0 , dimensionless	9.41E+05	1.84E+07	$K_{ow}(283.15) = K_{ow}^0(298.15) \exp(a_{Kow}(1/T - 1/T_0))$, where $K_{ow}^0(298.15) = 5.13E+5$; 1.54E+7 for PCB-28 and 180 respectively; $a_{Kow} = dHK_{ow}/R$ dHK_{ow} = phase transfer enthalpy (J/mol) PCB 28: -28400; PCB 180: -8270 R = universal gas constant (8.3145 J/mol·K)	Beyer et al., 2002
		a_{Kow}	3414.5	994.6		
		T_0, K	283.15	283.15		
MSCE-POP	Temperature independent	K_{ow} , dimensionless	6.31E+5	2.29E+7	PCB-28: $\log K_{ow} = 5.8$ PCB-180: $\log K_{ow} = 7.36$	Mackay et al., 1992; Hawker and Connell, 1988

* - for the sake of comparability, the base values and coefficients of temperature dependences of the considered parameters are given here for the temperature 283.15 K (T_0) and the way they were recalculated from original dependencies is specified in the field "Comments".

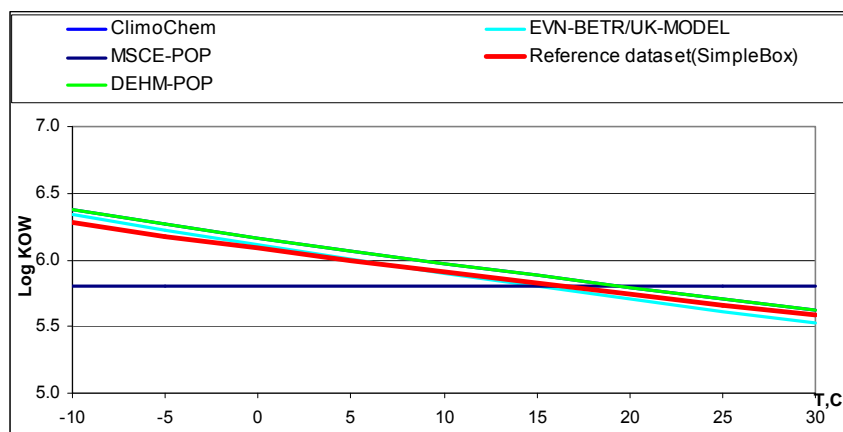


Fig. B.5. Comparison of temperature dependencies of $\log K_{ow}$ of PCB-28 used in the models and in “reference data set”

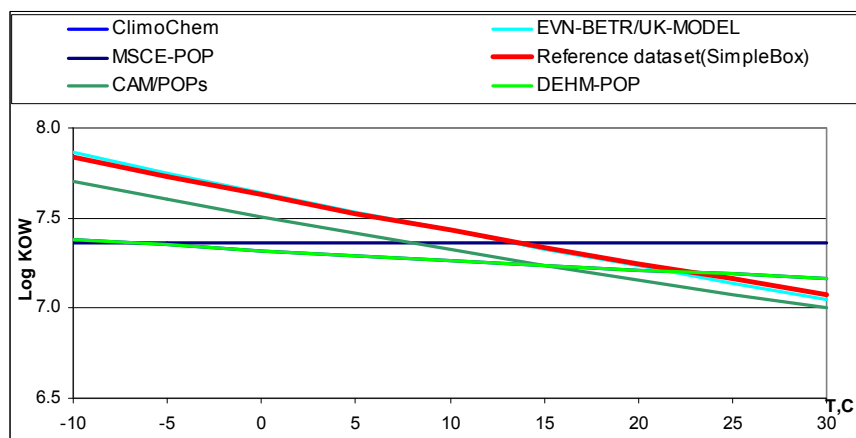


Fig. B.6. Comparison of temperature dependencies of $\log K_{ow}$ of PCB-180 used in the models and in “reference data set”

Table B.9. Absolute values, coefficients of temperature dependence and statistical parameters of octanol/water partition coefficient of PCB-28 for three arbitrary temperatures (-10 °C, 10 °C and 25 °C)

	K_{ow}			$a_{K_{ow}}$
	-10°C	10°C	25°C	
SimpleBox	1.89E+06	8.09E+05	4.61E+05	3163.3
EVN-BETR/UK-MODEL	2.19E+06	8.02E+05	4.13E+05	3740.5
CliMoChem	2.35E+06	9.41E+05	5.13E+05	3415.7*
DEHM-POP	2.35E+06	9.41E+05	5.13E+05	3414.5*
MSCE-POP	6.31E+05	6.31E+05	6.31E+05	-
Reference data set	1.89E+06	8.09E+05	4.61E+05	3163.3
<i>min</i>	6.31E+05	6.31E+05	4.13E+05	3163.3
<i>max</i>	2.35E+06	9.41E+05	6.31E+05	3740.5
<i>arith. mean</i>	1.88E+06	8.25E+05	5.06E+05	3433.5
<i>median</i>	2.19E+06	8.09E+05	5.13E+05	3415.1
<i>geom. mean</i>	1.71E+06	8.16E+05	5.01E+05	3427.4
<i>max/min</i>	1.2/3.7**	1.2/1.5**	1.2/1.5**	1.2

* - difference in absolute values obtained for identical temperature dependencies can be explained by accuracy of coefficient recalculation;

** - the first value is calculated without the temperature independent value of K_{ow} (MSCE-POP), the second value is calculated taking it into account

Table B.10. Absolute values, coefficients of temperature dependence and statistical parameters of octanol/water partition coefficient of PCB-180 for three arbitrary temperatures (-10 °C, 10 °C and 25 °C)

	K_{ow}			$a_{K_{ow}}$
	-10°C	10°C	25°C	
CAM/POPs	5.11E+07	2.12E+07	1.20E+07	-
SimpleBox	6.91E+07	2.70E+07	1.45E+07	3500.1*
EVN-BETR/UK-MODEL	7.34E+07	2.69E+07	1.38E+07	3740.5*
CliMoChem	2.40E+07	1.84E+07	1.54E+07	994.6
DEHM-POP	2.40E+07	1.84E+07	1.54E+07	994.6
MSCE-POP	2.29E+07	2.29E+07	2.29E+07	-
Reference data set	6.91E+07	2.70E+07	1.45E+07	3500.1*
<i>min</i>	2.29E+07	1.84E+07	1.20E+07	994.6
<i>max</i>	7.34E+07	2.70E+07	2.29E+07	3740.5
<i>arith. mean</i>	4.27E+07	2.27E+07	1.64E+07	2307.5
<i>median</i>	2.40E+07	2.29E+07	1.54E+07	2247.4
<i>geom. mean</i>	3.68E+07	2.24E+07	1.61E+07	1897.0
<i>max/min</i>	3.1/3.2**	1.5/1.5**	1.3/1.9**	3.8

* - difference in absolute values obtained from identical temperature dependencies can be explained by accuracy of coefficient recalculation

** - the first value is calculated without the temperature independent value of K_{ow} (MSCE-POP), the second value is calculated taking it into account

Table B.11. The octanol/air partition coefficient of PCBs (data sets of the participating POP models)*

Model	Description	Numerical values			Comments	Reference
			PCB-28	PCB-180		
CAM/POPs	Temperature dependent: $K_{oa} = 10^{(a/T + b)}$ where T - temperature; P - liquid vapour pressure p_{ol} (Pa)	a	-	-529-19.25 logP	These values are calculated with the help of temperature dependencies of p_{ol}	Harner et al, 1996; 1998
		b	-	8.2995-0.95 logP		
SimpleBox	Temperature dependent: $K_{oa} = K_{oa}^0 \exp(a_{Koa}(1/T - 1/T_0))$ where T - temperature (K), K_{oa}^0 is the value at the reference temperature T_0 , and a_{Koa} is a parameter of temperature dependence.	$K_{oa}^0(T_0)$, dimensionless	3.77E+08	1.06E+11	Same to the "reference data set"	Li et al., 2003
		a_{Koa}	9441.9	11161.9		
		T_0, K	283.15	283.15		
EVN-BETR and UK-MODEL	Temperature dependent:	$K_{oa}^0(T_0)$, dimensionless	1.99E+08	3.18E+10	At 10°C, calculated as $K_{oa} = K_{ow} / K_{aw}$	
		T_0, K	283.15	283.15		
DEHM-POP	Temperature dependent: $K_{oa} = K_{oa}^0 \exp(a_{Koa}(1/T - 1/T_0))$ where T - temperature (K), K_{oa}^0 is the value at the reference temperature T_0 , and a_{Koa} is a parameter of temperature dependence.	$K_{oa}^0(T_0)$, dimensionless	5.84E+08	9.78E+10	$K_{oa}(283.15) = K_{oa}^0(298.15) \exp(a_{Koa}(1/T - 1/T_0))$, where $K_{oa}^0(298.15) = 1.16E+8, 1.68E+10$ for PCB-28 and 180 respectively $a_{Koa} = dHK_{oa}/R$ dHK_{oa} = phase transfer enthalpy (J/mol) PCB 28: -75620; PCB-180: -82410 R = universal gas constant (8.3145 J/mol-K)	Beyer et al., 2002
		a_{Koa}	9095.0	9911.6		
		T_0, K	283.15	283.15		
MSCE-POP	Temperature dependent: $K_{oa} = K_{oa}^0 \exp(a_{Koa}(1/T - 1/T_0))$ where T - temperature (K), K_{oa}^0 is the value at the reference temperature T_0 , and a_{Koa} is a parameter of temperature dependence.	$K_{oa}^0(T_0)$, dimensionless	5.78E+8	2.07E+11	Coefficients of the exponential equation are recalculated from the standard form of temperature dependence: $\log K_{oa} = A/T(K) - B$ with the help of the following formulas: $a_p = \ln(10) \cdot A$, $K_{oa}^0(T_0) = 10^{(A/T_0 - B)}$ where: $A = 3792^a$ and 4535^b for PCB-28 and PCB-180 respectively; $B = 4.63^a$ and 4.70^b for PCB-28 and PCB-180 respectively	^a -estimated with the use of data [Harner and Bidleman 1996] for PCB-29 ^b -Harner and Bidleman [1996]
		a_{Koa}	8731	10442		
		T_0, K	283.15	283.15		

* - for the sake of comparability, the base values and coefficients of temperature dependences of the considered parameters are given here for the temperature 283.15 K (T_0) and the way they were recalculated from original dependencies is specified in the field "Comments".

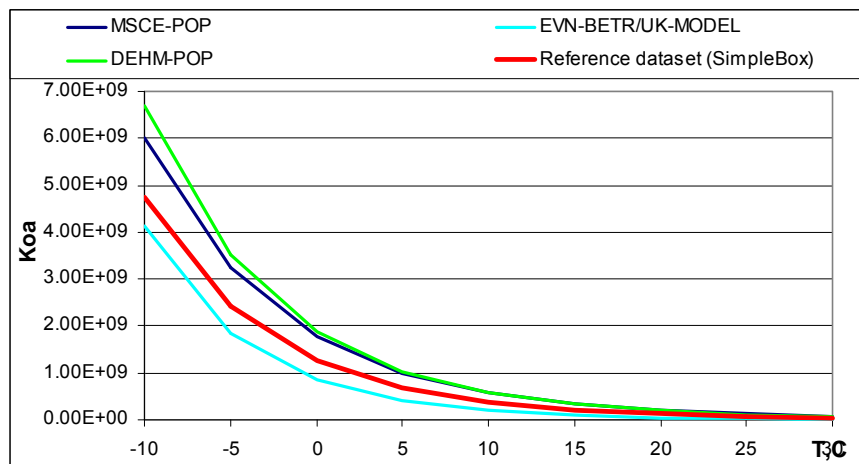


Fig. B.7. Comparison of temperature dependencies of octanol/air partition coefficient of PCB-28 used in the participating POP models and in “reference data set”

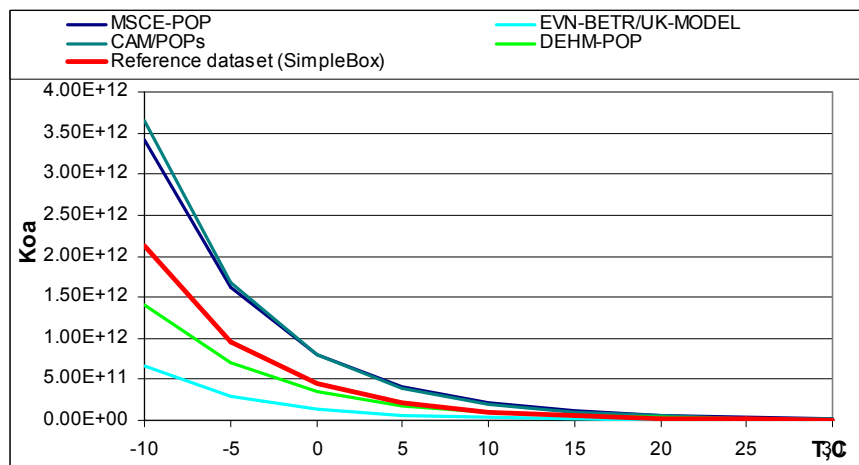


Fig. B.8. Comparison of temperature dependencies of octanol/air partition coefficient of PCB-180 used in the participating POP models and in “reference data set”

Table B.12. Absolute values, coefficients of temperature dependencies and statistical parameters of octanol/air partition coefficient of PCB-28 for three arbitrary temperatures (-10 °C, 10 °C and 25 °C)

	K_{oa}			$a_{K_{oa}}$
	-10°C	10°C	25°C	
SimpleBox	4.75E+09	3.77E+08	7.04E+07	9441.9
EVN-BETR/UK-MODEL	4.14E+09	2.00E+08	2.68E+07	-
DEHM-POP	6.71E+09	5.84E+08	1.16E+08	9095.0
MSCE-POP	6.02E+09	5.78E+08	1.23E+08	8731
Reference data set	4.75E+09	3.77E+08	7.04E+07	9441.9
<i>min</i>	4.14E+09	2.00E+08	2.68E+07	8731.0
<i>max</i>	6.71E+09	5.84E+08	1.23E+08	9441.9
<i>arith. mean</i>	5.27E+09	4.23E+08	8.12E+07	9177.5
<i>mediana</i>	4.75E+09	3.77E+08	7.04E+07	9268.5
<i>geom. mean</i>	5.19E+09	3.95E+08	7.17E+07	9172.7
<i>max/min</i>	2	3	5	1.1

Table B.13. Absolute values, coefficients of temperature dependencies and statistical parameters of octanol/air partition coefficient of PCB-180 for three arbitrary temperatures (-10 °C, 10 °C and 25 °C)

	K_{oa}			$a_{K_{oa}}$
	-10°C	10°C	25°C	
CAM/POPs	3.65E+12	1.97E+11	2.91E+10	-
SimpleBox	2.12E+12	1.06E+11	1.46E+10	11161.9
EVN-BETR/UK-MODEL	6.58E+11	3.17E+10	4.26E+09	-
DEHM-POP	1.40E+12	9.78E+10	1.68E+10	9911.6
MSCE-POP	3.41E+12	2.07E+11	3.24E+10	10442
Reference data set	2.12E+12	1.06E+11	1.46E+10	11161.9
<i>min</i>	6.58E+11	3.17E+10	4.26E+09	9911.6
<i>max</i>	3.65E+12	2.07E+11	3.24E+10	11161.9
<i>arith. mean</i>	2.23E+12	1.10E+11	1.65E+10	10669.4
<i>mediana</i>	2.12E+12	1.06E+11	1.46E+10	10802.0
<i>geom. mean</i>	1.93E+12	9.37E+10	1.38E+10	10656.2
<i>max/min</i>	6	7	8	1.1

Table B.14. The organic carbon/water partition coefficient of PCBs (data sets of the participating POP models)

Model	Description	Numerical values			Comments	Reference
			PCB-28	PCB-180		
CAM/POPs	Regression relation: $K_{oc} = regc K_{ow}^b$ where <i>regc</i> and <i>b</i> are regression coefficients	<i>regc</i>	-	0.41	K_{oc} is calculated from K_{ow} , where K_{ow} is the temperature dependent octanol-water partition coefficient	Karickhoff, 1981; Mackay, 1991; Schnoor, 1996
		<i>b</i>	-	1		
SimpleBox	Regression relation: $K_{oc} = regc K_{ow}^b$ where <i>regc</i> and <i>b</i> are regression coefficients	<i>regc</i>	0.41	0.41	Same to the “reference data set” K_{oc} is calculated from K_{ow} , where K_{ow} is the temperature dependent octanol-water partition coefficient	Karickhoff, 1981
		<i>b</i>	1	1		
EVN-BETR and UK- MODEL	Regression relation: $K_{oc} = regc K_{ow}^b$ where <i>regc</i> and <i>b</i> are regression coefficients	<i>regc</i>	0.41	0.41		Karickhoff, 1981
		<i>b</i>	1	1		
CliMoChem	Regression relation: $K_{oc} = regc K_{ow}^b$ where <i>regc</i> and <i>b</i> are regression coefficients	<i>regc</i>	0.35	0.35	K_{oc} is calculated from K_{ow} , where K_{ow} is the temperature dependent octanol-water partition coefficient	Seth et al., 1999
		<i>b</i>	1	1		
DEHM-POP	Regression relation: $K_{oc} = regc K_{ow}^b$ where <i>regc</i> and <i>b</i> are regression coefficients	<i>regc</i>	0.41	0.41		Mackay, 1999
		<i>b</i>	1	1		
MSCE-POP	Regression relation: $K_{oc} = regc K_{ow}^b$ where <i>regc</i> and <i>b</i> are regression coefficients	<i>regc</i>	0.41	0.41		Karickhoff, 1981
		<i>b</i>	1	1		

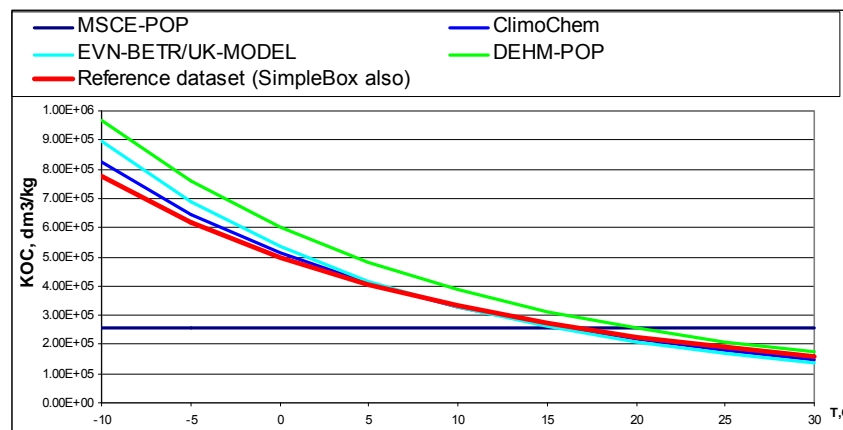


Fig. B.9. Comparison of temperature dependencies of organic carbon/water partition coefficient of PCB-28 used in the participating POP models and in “reference data set”

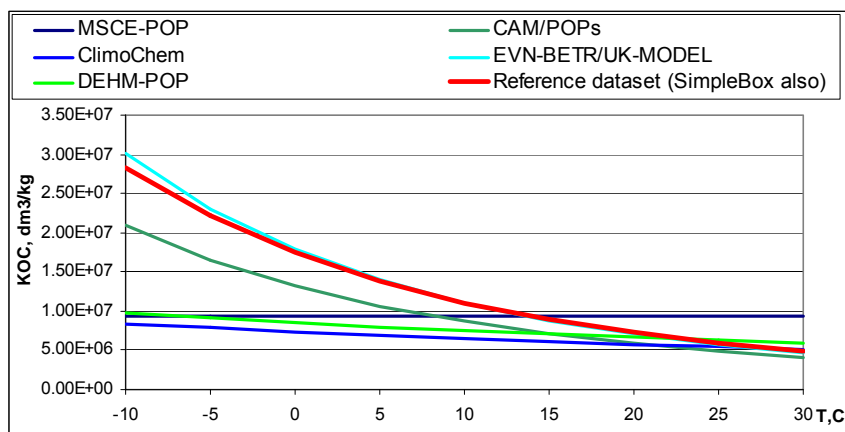


Fig. B.10. Comparison of temperature dependencies of organic carbon/water partition coefficient of PCB-180 used in the participating POP models and in “reference data set”

Table B.15. Absolute values and statistical parameters of organic carbon/water partition coefficient of PCB-28 for three arbitrary temperatures (-10 °C, 10 °C and 25 °C).

	K_{oc} , dm ³ /kg		
	-10°C	10°C	25°C
SimpleBox	7.75E+05	3.32E+05	1.89E+05
EVN-BETR/UK-MODEL	8.97E+05	3.29E+05	1.69E+05
CliMoChem	8.24E+05	3.29E+05	1.80E+05
DEHM-POP	9.65E+05	3.86E+05	2.10E+05
MSCE-POP	2.59E+05	2.59E+05	2.59E+05
Reference data set	7.75E+05	3.32E+05	1.89E+05
<i>min</i>	2.59E+05	2.59E+05	1.69E+05
<i>max</i>	9.65E+05	3.86E+05	2.59E+05
<i>arith. mean</i>	7.49E+05	3.28E+05	1.99E+05
<i>mediana</i>	8.00E+05	3.31E+05	1.89E+05
<i>geom. mean</i>	6.93E+05	3.25E+05	1.97E+05
<i>max/min</i>	3.7	1.5	1.5

Table B.16. Absolute values and statistical parameters of organic carbon/water partition coefficient of PCB-180 for three arbitrary temperatures (-10 °C, 10 °C and 25 °C).

	K_{oc} , dm ³ /kg		
	-10°C	10°C	25°C
CAM/POPs	2.09E+07	8.68E+06	4.92E+06
SimpleBox	2.83E+07	1.11E+07	5.94E+06
EVN-BETR/UK-MODEL	3.01E+07	1.10E+07	5.67E+06
ClMoChem	8.41E+06	6.44E+06	5.40E+06
DEHM-POP	9.85E+06	7.54E+06	6.32E+06
MSCE-POP	9.39E+06	9.39E+06	9.39E+06
Reference data set	2.83E+07	1.11E+07	5.94E+06
<i>min</i>	8.41E+06	6.44E+06	4.92E+06
<i>max</i>	3.01E+07	1.11E+07	9.39E+06
<i>arith. mean</i>	1.93E+07	9.32E+06	6.23E+06
<i>mediana</i>	2.09E+07	9.39E+06	5.94E+06
<i>geom. mean</i>	1.69E+07	9.15E+06	6.10E+06
<i>max/min</i>	3.6	1.7	1.9

Table B.17. Water solubility of PCBs (data sets of the participating POP models)

Model	Description	Numerical values			Comments	Reference
			PCB-28	PCB-180		
SimpleBox	Temperature independent	$S_{WL}(T)$, mol/m ³	5.53E-04	7.57E-06	Same to the "reference data set" $T = 10\text{ }^{\circ}\text{C}$	<i>Li et al.</i> , 2003
EVN-BETR and UK-MODEL	Temperature independent.	$S_{WL}(T)$, mol/m ³	8.85E-04	1.32E-05	$T = 25\text{ }^{\circ}\text{C}$	<i>Li et al.</i> , 2003

Table B.18. Degradation rate constants of PCBs in the environmental media (data sets of the participating POP models)*

Model	Description	Numerical values			Comments	Reference
			PCB-28	PCB-180		
CAM/POPs	Degradation in atmosphere: Temperature dependent: $k_{air} = k_{air}^0 \exp (-a_{kair}(1/T - 1/T_0))$ where T - temperature (K), k_{air}^0 is the value at the reference temperature T_0 , and a_{kair} is a parameter of temperature dependence	$k_{air}^0 T_0$, cm ³ /molec·s	-	1.25E-13	Coefficients of the exponential equation are recalculated from the following temperature dependence: $K_{OH} = K_{OH}^0 \exp(a(1/T_0 - 1/T))$ where $K_{OH}^0 = 1.6E-13$ is the value at the reference temperature T_0 (298 K), $a = 1400$ is parameter of temperature dependence.	This study
		a_{kair}	-	1400		
		T_0, K	-	283.15		
CliMoChem	Degradation in atmosphere: Temperature dependent: $k_{air} = k_{air}^0 \exp (-a_{kair}(1/T - 1/T_0))$ where T - temperature (K), k_{air}^0 is the value at the reference temperature T_0 , and a_{kair} is a parameter of temperature dependence	$k_{air}^0 (T_0)$, cm ³ /molec·s	7.95E-13	7.15E-14	$k_{air}(T) = k_{air}(T_{ref}) \exp((Ea_{air}/R)(1/T - 1/T_0))$ T = temperature (283.15 K), T_0 = reference temperature (298.15 K) $k_{air}(T_0)$ = degradation rate constant at T_0 (cm ³ /d), PCB 28: 9.21E-8 ; PCB 180: 9.04E-9 Ea_{air} = activation energy (J/mol) PCB 28: 13700; PCB 180: 17800 R = universal gas constant (8.3145 J/mol·K) k_{air}^0 = degradation rate constant at 283.15 (cm ³ /d), PCB 28: 6.87E-08; PCB-180: 6.18E-09 $a_{kair} = Ea/R$	Beyer et al., 2002
		a_{kair}	1647.7	2140.8		
		T_0, K	283.15	283.15		
	Degradation in soil: Temperature dependent: $k_{soil} = k_{soil}^0 \exp (-a_{ksoil}(1/T - 1/T_0))$ where T - temperature (K), k_{soil}^0 is the value at the reference temperature T_0 , and a_{ksoil} is a parameter of temperature dependence	$k_{soil}^0 (T_0)$, 1/d	3.90E-09	3.07E-10	$k_{soil}(T) = k_{soil}(T_{ref}) \exp((Ea_{soil}/R)(1/T - 1/T_0))$ T = temperature (283.15 K), T_0 = reference temperature (298.15 K) $k_{soil}(T_0)$ = degradation rate constant at T_0 (1/d), PCB 28: 6.40E-4 ; PCB 180: 5.04E-5 Ea_{soil} = activation energy (J/mol) PCB 28: 30000; PCB 180: 30000 R = universal gas constant (8.3145 J/mol·K) k_{soil}^0 = degradation rate constant at 283.15 (1/d) PCB 28: 3.37E-04; PCB-180: 2.65E-05 $a_{ksoil} = Ea_{soil}/R$	
		a_{ksoil}	3608.2	3608.2		
		T_0, K	283.15	283.15		
	Degradation in water: Temperature dependent: $k_{water} = k_{water}^0 \exp (-a_{kwater}(1/T - 1/T_0))$ where T - temperature (K), k_{water}^0 is the value at the reference temperature T_0 , and a_{kwater} is a parameter of temperature dependence	$k_{water}^0 (T_0)$, 1/d	7.01E-08	4.22E-10	$k_{water}(T) = k_{water}(T_{ref}) \exp((Ea_{water}/R)(1/T - 1/T_0))$ T = temperature (283.15 K), T_0 = reference temperature (298.15 K) $k_{water}(T_0)$ = degradation rate constant at T_0 (1/d), PCB 28: 1.15E-2 ; PCB 180: 6.93E-5 Ea_{water} = activation energy (J/mol) PCB 153: 30000; PCB 28: 30000 ; PCB 180: 30000 R = universal gas constant (8.3145 J/mol·K) k_{water}^0 = degradation rate constant at 283.15 (1/d), PCB 28: 6.06E-03; PCB-180: 3.65E-05 $a_{kwater} = Ea_{water}/R$	
		a_{kwater}	3608.2	3608.2		
		T_0, K	283.15	283.15		
	Degradation in vegetation*: Temperature dependent: $k_{veg} = k_{veg}^0 \exp (-a_{kveg}(1/T - 1/T_0))$ where T - temperature (K), k_{veg}^0 is the value at the reference temperature T_0 , and a_{kveg} is a parameter of temperature dependence	$k_{veg}^0 (T_0)$, 1/d	7.71E-07	6.94E-08	$k_{veg}(T) = k_{veg}(T_{ref}) \exp((Ea_{veg}/R)(1/T - 1/T_0))$ T = temperature (283.15 K), T_0 = reference temperature (298.15 K) $k_{veg}(T_0)$ = degradation rate constant at T_0 (1/d)*, PCB 28: 8.93E-2 ; PCB 180: 8.77E-3 Ea_{veg} = activation energy (J/mol) PCB 28: 13700 ; PCB 180: 17800 R = universal gas constant (8.3145 J/mol·K) $k_{veg}(T_0)$ = degradation rate constant at T_0 (1/d), PCB 28: 6.66E-02; PCB-180: 6.00E-03 $a_{kveg} = Ea_{veg}/R$	
		a_{kveg}	1647.7	2140.8		
		T_0, K	283.15	283.15		

Model	Description	Numerical values			Comments	Reference
			PCB-28	PCB-180		
MSCE-POP	Degradation in atmosphere: Temperature dependent: $k_{air} = k_{air}^0 \exp(-a_{kair}(1/T - 1/T_0))$ where T - temperature (K), k_{air}^0 is the value at the reference temperature T_0 , and a_{kair} is a parameter of temperature dependence	$k_{air}^0(T_0)$, cm ³ /(molec·s)	7.95E-13	7.16E-14	Coefficients of the exponential equation are recalculated from the following temperature dependence: $k_{air} = A \cdot \exp(-Ea/RT)$ with the help of the following formulas: $a_{kair} = Ea/R$, $k_{air}^0 = A \cdot \exp(-Ea/RT_0)$ where $A = 2.70 \text{ E-10}$ and 1.40 E-10 are the pre-exponential multiplier values for PCB-28 and PCB-180 respectively, m ³ /(molec·s); $E_A = 13720$ and 17840 are the activation energies of interaction with OH-radical in air for PCB-28 and PCB-180 respectively, J/mol	<i>Anderson and Hites, 1996; Beyer and Matthies, 2001</i>
		a_{kair}	1650.1	2145.6		
		T_0, K	283.15	283.15		
	Degradation in soil: Temperature independent	$k_{soil}, 1/s$	7.4E-09	5.83E-10	Degradation rate constant in soil is converted from half-life values (PCB-28: 26000 hours; PCB-180: 330000 hours): $k_d = 0.693/ t_{1/2}$ where k_d is the first-order rate constant (s ⁻¹) and $t_{1/2}$ is the half-life (s).	<i>Sinkkonen and Paasivirta, 2000</i>
	Degradation in water: Temperature independent	$k_{water}, 1/s$	1.33E-07	8.02E-10	Degradation rate constant in water is converted from half-life values (PCB-28: 1450 hours; PCB-180: 240000 hours): $k_d = 0.693/ t_{1/2}$ where k_d is the first-order rate constant (s ⁻¹) and $t_{1/2}$ is the half-life (s).	
SimpleBox	Degradation in atmosphere: Temperature independent	$k_{air}, 1/s$	3.50E-07	3.50E-08	Same half-lives as in "reference data set": PCB-28: 550; PCB-180: 5500 hours	<i>Mackay et al. 1992</i>
	Degradation in soil: Temperature independent	$k_{soil}, 1/s$	3.50E-09	3.50E-09	Same half-lives as in "reference data set": PCB-28: 55000; PCB-180: 55000 hours	
	Degradation in water: Temperature independent	$k_{water}, 1/s$	1.13E-08	3.50E-09	Same half-lives as in "reference data set": PCB-28: 17000; PCB-180: 55000 hours	
EVN-BETR and UK-MODEL	Degradation in atmosphere: Temperature independent	$k_{air}, 1/s$	3.50E-07	3.50E-08	Same half-lives as in "reference data set": PCB-28: 550; PCB-180: 5500 hours	<i>Mackay et al. 1992</i>
	Degradation in soil: Temperature independent	$k_{soil}, 1/s$	3.50E-09	3.50E-09	Same half-lives as in "reference data set": PCB-28: 55000; PCB-180: 55000 hours	
	Degradation in water: Temperature independent	$k_{water}, 1/s$	1.13E-08	3.50E-09	Same half-lives as in "reference data set": PCB-28: 17000; PCB-180: 55000 hours	
	Degradation in sediment: Temperature independent	$k_{sed}, 1/s$	3.50E-09	3.50E-09	Same half-lives as in "reference data set": PCB-28: 55000; PCB-180: 55000 hours	
	Degradation in vegetation: Temperature independent	$k_{veg}, 1/s$	1.13E-07	1.13E-08	Half-lives: PCB-28: 1700; PCB-180: 17000 hours	

* - for the sake of comparability, the base values and coefficients of temperature dependences of the considered parameters are given here at the temperature 283.15 K (T_0) and the way they were recalculated from original dependencies is specified in the field "Comments".

** - because of insufficient data about vegetation degradation rate constants, the values are taken from atmospheric degradation [Möller, 2002] and multiplied with an average OH-radical concentration of 970000 1/cm³ [Beyer et al., 2002].

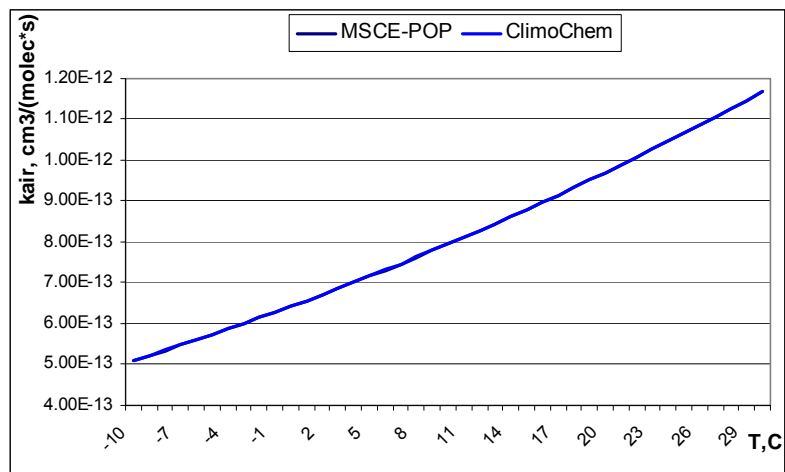


Fig. B.11. Comparison of temperature dependencies of degradation rate constant of PCB-28 in the atmosphere

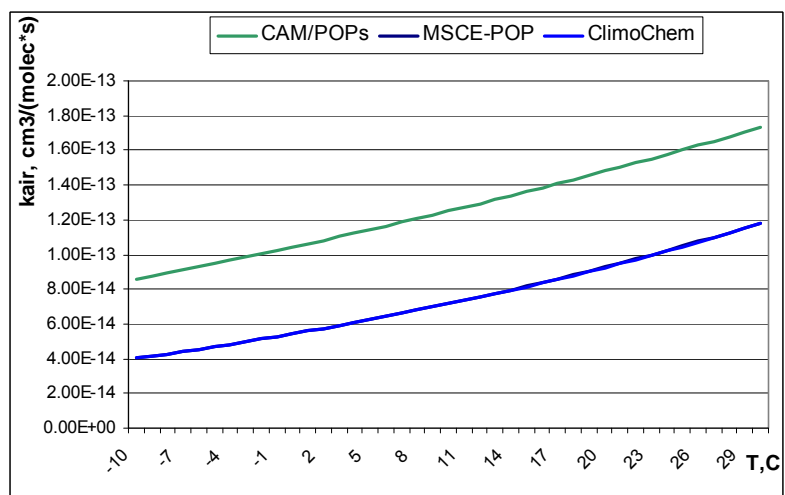


Fig. B.12. Comparison of temperature dependencies of degradation rate constant of PCB-180 in the atmosphere

Table B.19. Monthly averaged temperatures calculated on the basis of meteorological data for 1997, 1998 and 1999 in Europe and the yearly average degradation rate constants of PCB-28 for the models which use temperature dependence of this parameter

Month	Temperatures, °C			MSCE-POP	CliMoChem				
	Over land	Over sea	Average	air, $\text{cm}^3 \cdot \text{molec}^{-1} \cdot \text{s}^{-1}$	air, $\text{cm}^3 \cdot \text{molec}^{-1} \cdot \text{s}^{-1}$	soil, s^{-1} (for Over land temp)	sea, s^{-1} (for Over sea temp)	veg., s^{-1} (for aver. temp)	
Jan	4	4	4	7.01E-13	7.01E-13	2.96E-09	5.32E-08	6.80E-07	
Feb	4	3	4	7.01E-13	7.01E-13	2.96E-09	5.08E-08	6.80E-07	
Mar	7	5	6	7.31E-13	7.31E-13	3.4E-09	5.57E-08	7.09E-07	
Apr	11	6	9	7.79E-13	7.79E-13	4.08E-09	5.84E-08	7.55E-07	
May	17	10	13	8.45E-13	8.45E-13	5.3E-09	7.01E-08	8.20E-07	
Jun	21	14	17	9.15E-13	9.15E-13	6.28E-09	8.37E-08	8.87E-07	
Jul	22	16	19	9.51E-13	9.51E-13	6.55E-09	9.13E-08	9.22E-07	
Aug	22	16	19	9.51E-13	9.51E-13	6.55E-09	9.13E-08	9.22E-07	
Sep	18	13	15	8.8E-13	8.79E-13	5.54E-09	8.01E-08	8.53E-07	
Oct	14	10	12	8.28E-13	8.28E-13	4.66E-09	7.01E-08	8.03E-07	
Nov	10	7	9	7.79E-13	7.79E-13	3.9E-09	6.12E-08	7.55E-07	
Dec	6	5	6	7.31E-13	7.31E-13	3.25E-09	5.57E-08	7.09E-07	
Averaged second-order rate constants, $\text{cm}^3 \cdot \text{molec}^{-1} \cdot \text{s}^{-1}$				8.16E-13	8.16E-13	-	-	-	
Averaged first-order rate constants, s^{-1}				6.53E-07	6.53E-07	4.62E-09	6.85E-08	7.92E-07	

Table B.20. Absolute values and statistical parameters of degradation rate constants of first order (PCB-28)

	$k_{\text{air}}, \text{s}^{-1}$	$k_{\text{soil}}, \text{s}^{-1}$	$k_{\text{water}}, \text{s}^{-1}$	$k_{\text{sediment}}, \text{s}^{-1}$	$k_{\text{veg}}, \text{s}^{-1}$
CliMoChem	6.53E-07	4.62E-09	6.85E-08	-	7.92E-07
MSCE-POP	6.53E-07	7.4E-09	1.33E-07	-	-
SimpleBox	3.50E-07	3.50E-09	1.13E-08	-	-
EVN-BETR/UK-MODEL	3.50E-07	3.50E-09	1.13E-08	3.50E-09	1.13E-07
Reference data set	3.50E-07	3.50E-09	1.13E-08	3.50E-09	-
<i>min</i>	3.50E-07	3.50E-09	1.13E-08	-	-
<i>max</i>	6.53E-07	7.40E-09	1.33E-07	-	-
<i>arith. mean</i>	4.71E-07	4.50E-09	4.71E-08	-	-
<i>median</i>	3.50E-07	3.50E-09	1.13E-08	-	-
<i>geom.mean</i>	4.49E-07	4.30E-09	2.65E-08	-	-
<i>max/min</i>	1.9	2.1	11.8	1.0	7.0

Table B.21. Monthly averaged temperatures calculated on the basis of meteorological data for 1997, 1998 and 1999 in Europe and the yearly average degradation rate constants of PCB-180 for the models which use temperature dependence of this parameter

Month	Temperatures, °C			CAM/POPs	MSCE-POP	CliMoChem			
	Over land	Over sea	Average	air, $\text{cm}^3 \cdot \text{molec}^{-1} \cdot \text{s}^{-1}$	air, $\text{cm}^3 \cdot \text{molec}^{-1} \cdot \text{s}^{-1}$	air, $\text{cm}^3 \cdot \text{molec}^{-1} \cdot \text{s}^{-1}$	soil, s^{-1} (for Over land temp)	sea, s^{-1} (for Over sea temp)	veg., s^{-1} (for aver. temp)
Jan	4	4	4	1.12E-13	6.08E-14	6.07E-14	2.33E-10	3.2E-10	5.89E-08
Feb	4	3	4	1.12E-13	6.08E-14	6.07E-14	2.33E-10	3.06E-10	5.89E-08
Mar	7	5	6	1.16E-13	6.42E-14	6.42E-14	2.68E-10	3.36E-10	6.23E-08
Apr	11	6	9	1.23E-13	6.97E-14	6.96E-14	3.21E-10	3.52E-10	6.76E-08
May	17	10	13	1.32E-13	7.75E-14	7.74E-14	4.17E-10	4.22E-10	7.51E-08
Jun	21	14	17	1.41E-13	8.6E-14	8.58E-14	4.94E-10	5.04E-10	8.33E-08
Jul	22	16	19	1.46E-13	9.04E-14	9.03E-14	5.15E-10	5.5E-10	8.76E-08
Aug	22	16	19	1.46E-13	9.04E-14	9.03E-14	5.15E-10	5.5E-10	8.76E-08
Sep	18	13	15	1.36E-13	8.17E-14	8.15E-14	4.36E-10	4.82E-10	7.91E-08
Oct	14	10	12	1.29E-13	7.55E-14	7.54E-14	3.67E-10	4.22E-10	7.32E-08
Nov	10	7	9	1.23E-13	6.97E-14	6.96E-14	3.07E-10	3.68E-10	6.76E-08
Dec	6	5	6	1.16E-13	6.42E-14	6.42E-14	2.56E-10	3.36E-10	6.23E-08
Averaged second-order rate constants, $\text{cm}^3 \cdot \text{molec}^{-1} \cdot \text{s}^{-1}$				1.28E-13	7.42E-14	7.41E-14	-	-	-
Averaged first-order rate constants, s^{-1}				1.02E-07	5.94E-08	5.93E-08	3.64E-10	4.13E-10	7.19E-08

Table B.22. Absolute values and statistical parameters of degradation rate constants of first order (PCB-180)

	$k_{\text{air}}, \text{s}^{-1}$	$k_{\text{soil}}, \text{s}^{-1}$	$k_{\text{water}}, \text{s}^{-1}$	$k_{\text{sediment}}, \text{s}^{-1}$	$k_{\text{veg.}}, \text{s}^{-1}$
CAM/POPs	1.02E-07	-	-	-	-
CliMoChem	5.93E-08	3.64E-10	4.13E-10	-	7.19E-08
MSCE-POP	5.94E-08	5.83E-10	8.02E-10	-	-
SimpleBox	3.50E-08	3.50E-09	3.50E-09	-	-
EVN-BETR/UK-MODEL	3.50E-08	3.50E-09	3.50E-09	3.50E-09	1.13E-08
Reference data set	3.50E-08	3.50E-09	3.50E-09	3.50E-09	-
<i>min</i>	3.50E-08	3.64E-10	4.13E-10	-	-
<i>max</i>	1.02E-07	3.50E-09	3.50E-09	-	-
<i>arith. mean</i>	5.43E-08	2.29E-09	2.34E-09	-	-
<i>median</i>	4.72E-08	3.50E-09	3.50E-09	-	-
<i>geom.mean</i>	4.99E-08	1.56E-09	1.70E-09	-	-
<i>max/min</i>	2.9	9.6	8.5	1.0	6.4